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Experimental assessment of a CI engine operating with 1-pentanol/diesel fuel blends

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Abstract

Alcohols have been known as influential alternatives for the utilization in the compression-ignition (CI) engines. In contrast to lower-order alcohols such as methanol-C1 and ethanol-C2, long-chain alcohols (higher-order alcohols) have a hopeful future for CI engines. Pentanol-C5 or amyl alcohol, regarding its affirmative chemical and physical properties, is a type of higher alcohol that can be obtained from biomass resources and hence it has to be evaluated as an alternating and sustainable fuel candidate in diesel engine applications. The objective of this work is to explore the engine performance and exhaust emission characteristics of a CI engine running on 1-pentanol/diesel fuel mixtures. For this aim of the experimental research, three different blends were created by infusing various ratios (10, 20, and 30% by volume) of 1-pentanol into pure diesel with implementing the splash-blending method to acquire the binary blends of Pt10, Pt20, and Pt30. The tested fuel samples were used in a single-cylinder diesel engine coupled with a generator. The influences of a next-generation alcohol addition to the diesel upon the engine performance along with exhaust emission levels of the tested engine were meticulously researched at six different engine loads (0, 0.4, 0.8, 1.2, 1.6, and 2 kW) with a stable speed (3000 rpm). The infusion of alcohol into the diesel fuel declined cetane number as well as the lower calorific value of the fuel blends. As a result of the study carried out, it was observed that the brake specific fuel consumption (BSFC) increased between 4.46-11.78% averagely as the ratio of 1-pentanol in the mixtures increased while brake thermal efficiency (BTE) and exhaust gas temperature (EGT) dropped up to 6.75% and 6.69%, respectively owing to the lesser energy content of the 1-pentanol. When the test engine operating with binary blends, unburned hydrocarbon (HC) and carbon monoxide (CO) emissions were obtained to be higher than that of conventional diesel fuel due to the higher latent heat of vaporization (LHV) of 1-pentanol resulting in a cooling impact in the cylinder, leading descending trend in the efficiency of the combustion. Besides, the addition of 1-pentanol to diesel caused the mitigation in smoke emission by 77.37-89.60%, carbon dioxide (CO₂) by 13.06-30.83%, and nitrogen oxides (NO_x) by 13.43-41.61% on an average as compared to diesel fuel. Overall, it has been shown up that 1-pentanol might be successfully utilized as an oxygenated fuel additive to diesel fuel, however in a minimum concentration of 1-pentanol, i.e., Pt10 blend has provided luminous outcomes in terms of mitigating the EGT, smoke opacity, and especially NO_x emissions, however at the expense of boosting in the emissions of CO and HC.

Keywords: Diesel engine; Emissions; Higher alcohol; 1-Pentanol; Performance

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1. Introduction

An average of 85 million barrels of oil has been consumed daily due to increasing energy needs in recent years all over the world. The energy consumption speed around the world is about 300 thousand times higher than the speed of the formation of fossil-based fuels [1]. It is estimated that crude oil will be depleted in the next 50 years [2]. Therefore, the researches and development studies have continued for alternative and clean fuels that will replace crude oil. The search for alternative fuels has taken an important place in the world agenda in previous years [3]. The oil embargo declared by the Organization of Arab Petroleum Exporting Countries (OAPEC) against the USA, which supported Israel in the Arab-Israeli War, on October 15, 1973, is known as the Oil Crisis or the 1973 crisis [4]. Since the industrialized countries are the most important customers of oil exporters, this serious crisis has focused the researchers on the seek for alternative energy sources for the first time [5].

Nowadays, the augmentation in the number of motor vehicles has led to a faster depletion of fossil-based fuels with limited resources. Overconsumption of fossil-based fuels has caused oil wars and environmental problems in the world [6]. Global climate change and global warming have been threatening the countries. One of the main reasons for climate change is to be noted the increased usage of fossil-based fuels. Thus, researchers aim to utilize the alternative fuels instead of fossil-based fuels by making direct changes to fuel and without making too many changes in fuel systems [7-9]. Liquefied petroleum gas (LPG), Compressed natural gas (CNG), Alcohol-based fuels, Biodiesel, Biogas, and Hydrogen are used as alternative fuels instead of fossil-based fuels in vehicles powered by the internal combustion engines [10, 11]. In order to prefer a fuel as an alternative, a) it should not require too many changes in the fuel systems of the engine, b) it should not cause an excessive decrease in performance, c) it should decrease exhaust emissions, and d) it should be economically affordable [12].

Dropping the levels of air pollution all over the world is complicated and therefore, it requires some factors like awareness of humans, progress in the technology, and policy precautions. Some of the Eastern European countries have recommended limitations or even the forbid of the use of the vehicles powered with diesel engines, at least for light vehicles so as to decrease the levels of air pollution along with ensuring the low and ultra-low emission regions in the cities after the emission scandal in particular [13, 14]. It can be stated that many European countries, nonetheless, depend on fossil-based fuel sources heavily. There is still a long road in advance to attain low carbon energy systems even though the endeavors and alterations in the energy policies implemented by European countries [15]. Dey et al. [16] reported that prohibiting older cars, prohibiting new vehicles having diesel engines, rising the tax of the diesel

consumption, altering the motor tax to the prior engine capacity-based approximation have been effectual preventions for decreasing the influences considerably. However, abandon from diesel engines is not feasible in the near future due to the systems where high power is required such as heavy-duty vehicles, agricultural machines, power generation stations, etc. From this perspective, in the recent years, great progress has been made in diesel engine design and technology [17]. It has been noted by the majority of the researchers that the releasing of air pollutants from internal combustion engines may generally mitigate if alternative and clean fuels have been used instead of fossil-based pure diesel in these engines [18-20].

Biodiesel is an environmentally friendly and renewable fuel within the scope of biofuels that can be synthesized from comestible or non-comestible vegetable oils (canola, sunflower, safflower, cottonseed, mustard, soybean, etc.) and animal fats with the help of various chemical methods like dilution, pyrolysis, micro-emulsion, transesterification, etc. [21, 22]. The fact that biodiesel freezes faster, its properties such as high viscosity, the tendency to oxidation, and low energy content, and that it causes the increase of NO_x in exhaust emissions have led to problems in its direct use as an alternate fuel in the diesel engines [23-25]. Therefore, researchers have recommended using alcohol with better fuel characteristics and higher carbon chains as alternative fuels to solve these issues [10, 26, 27].

Ethyl and methyl alcohols have been known as the utmost surveyed and preferred alcohols as alternative fuels in the literature. For instance, Can et al. [28] looked into the influences of ethyl alcohol infusion (10% and 15% v/v) into No. 2 diesel on the emission and performance behaviors of a turbocharged indirect-injection (IDI) diesel engine under diverse pressures for injection like 150 bar, 200 bar, and 250 bar. The researchers indicated that the alcohol addition dropped the sulfur dioxide (SO_2), soot, and CO emissions even though it led to an augmentation in NO_x emission. The engine power decreased by pretty much 12.5% in 10% ethanol fraction and 20% in 15% ethanol fraction. Also, the increase of the fuel injection pressure in the engine fueled with diesel/ethanol mixtures caused declining smoke and CO as compared to diesel. Özgür et al. [29] analyzed the emissions, performance, and efficiency of a CI engine powered by ethanol/diesel blend which contains 20% ethanol on a volume basis. The experiments were carried out between 1000-2600 rpm engine speed. According to the results, specific fuel consumption, and NO_x emission augmented regarding the usage of diesel/alcohol blend while power, torque, and CO emission reduced. Besides, the alcohol addition to diesel allowed descending in both energy and exergy efficiencies. Khoobbakht et al. [30] executed the exergy and energy analysis of a CI engine running with the ternary mixtures of biodiesel, ethanol, and diesel fuel exerting central composite rotatable design of response surface methodology. The researchers found that 0.08 L etha-

nol/0.17 L biodiesel/1 L diesel blend showed the most exergy efficiency under the load of 94% with the speed of 1900 rpm. At the aforementioned conditions, the highest energy and exergy efficiency values were calculated to be as 36.61% and 33.81%, respectively. Interestingly, Chen et al. [31] performed on the emission and combustion features of a common-rail diesel engine fueled with the mixtures of diesel, n-pentanol, and methanol at different loads. The experimental results presented that the ignition delay extended, the period of combustion reduced, and the maximum temperature of the combustion process rose with the ascending of methanol concentration in the sample. In addition, the methanol addition caused to descend in soot intensity while the turn up in the emission of NO_x . Duraisamy et al. [32] conducted comparative work on methanol/polyoxymethylene dimethyl ethers and methanol/diesel dual blends upon the reactivity controlled CI burning features in an automotive engine having three-cylinder, four-stroke, and turbocharged properties under 3.4 bar brake mean effective pressure with 1500 rpm speed. The researchers were to be noted that brake specific oxides of nitrogen and soot emissions were substantially mitigated for both of the dual fuel with the increase in methanol mass fraction meanwhile CO and HC profiles were vaguely gone up. Pedrozo et al. [33] examined a lean-burn strategy of the combustion for diesel/ethanol blend to increase the efficiency and to go down the exhaust pollutants of the tested engine at a fixed speed (1200 rpm) along with different loading conditions from 0.3 to 2.4 MPa net indicated mean effective pressure (IMEP). Consequently, the findings coming from the experiments exhibited that dual-fuel combustion strategy by using a fuel involving low carbon like ethanol was a powerful aspect of declining the dependency on conventional diesel fuel and incorporated greenhouse gas emissions. Al-Esawi et al. [34] investigated the influence of ethanol/biodiesel/diesel ternary mixtures on some of the fuel characteristics. They observed that the blend of 18% soybean oil methyl ester, 5% ethanol, and 80% diesel resulted in a little alteration in cetane number, calorific value, viscosity, and droplet lifetime in comparison with the pure diesel fuel by 0.2%, 2.2%, 2.0%, and 1.2%, respectively.

The number of carbon atoms for alcohols determines their physical and chemical properties. The boiling point of alcohol is much higher compared to hydrocarbons, which have an equal number of carbon atoms because they contain hydrogen bonds between their molecules. Since alcohols contain one or more oxygen atoms, their combustion heat is lower. While methanol is produced from coal and petroleum derivatives, ethanol is obtained from biomass through fermentation process [35, 36]. Since methanol possesses a very restricted solubility characteristic inside of diesel, ethanol has been the most commonly used alternative fuel. In addition, ethanol has been easily exploited in both spark-ignition and CI engines out of any major modification on the engines. According to researches, when 5-30% ethanol

is added to pure diesel fuel, there are enhancements in fuel consumption and detracts in engine power [37, 38]. Besides that, ethanol causes combustion problems in engines because of its low flash point, boiling point, and viscosity properties.

Particle matter emissions have decreased when using oxygenated fuel additives as fuel in diesel engines. It is very important to use alcohol for reducing the pollutant emissions released from the engines to the environment [39]. However, it is not possible to use alcohols directly due to various fuel characteristics, especially the lower cetane number. The shaping of the fuel concoction, as well as combustion, occur simultaneously in diesel engines. The droplets that form the fuel blend in the consequence of spraying and the fuel/air mixture is not distributed homogeneously in the combustion chamber of the CI engine. For this reason, it does rather hard to create a homogeneous mix in diesel engines [40]. Actually, alcohols may be used by blends with pure diesel fuel with certain proportions without the need for modification in diesel engines. The alcohol that will form a mixture with diesel fuel must be dissolved in fuel at any rate and the stability of the mixture has to be ensured in all weather conditions.

Pentanol is a type of alcohol having five carbon atoms in its chemical structure, the molecular formula of which is $\text{C}_5\text{H}_{11}\text{OH}$. It has a moderate odor along with a colorless liquid. Its density is less than that of water [41, 42]. According to the physical properties of pentanol given in Table 1, it can be presumed to be an important additive to diesel amongst all mentioned alcohols.

Cetane number is an indication that shows the self-ignition quality of diesel fuel. A fuel with a high cetane number can ignite easily and burn quickly in the chamber of combustion. The cetane number of pentanol is upward than that of methanol and ethanol, as represented in Table 1 [46, 47]. The LCV, which is the energy amount indicator of the fuels used in the engines, is desired to be high. The LCV of pentanol is approximately 20% lower than that of traditional diesel because it contains oxygen [48]. Pentanol has a higher evaporation temperature than ethanol and methanol. Therefore, the evaporation and mixing of air with fuel are slower. High viscosity and density cause the fuel not to be atomically sprayed from the injector as anticipated [49, 50]. This case extends the ignition delay period that influences the reaction of the combustion taking place in the cylinder and causes poor combustion reaction. The density and viscosity values of pentanol are closer to diesel fuel than other alcohols. However, there are fewer studies on pentanol in the recent literature. A part of them have been summarized as follows: Ağbulut et al. [51] researched experimentally the utilization of fusel oil (isoamyl alcohol), that is one of the isomers of the pentanol, with diesel in a CI engine at four dissimilar loads (2.5, 5.0, 7.5, and 10 Nm) and at 2000 rpm engine speed. The researchers observed that the emissions of NO_x and CO remarkably descended down to 20%

and 52%, respectively

Table 1. Technical characterization of diesel and various alcohols [39, 43-45]

No	Properties	Unit	Methanol	Ethanol	Butanol	Pentanol	Diesel
1	Chemical formula	-	CH ₃ OH	C ₂ H ₅ OH	C ₄ H ₉ OH	C ₅ H ₁₁ OH	C _x H _y
2	Molecular weight	g/mol	32.04	46.07	74.12	88.15	190-211.7
3	Carbon	wt. %	37.48	52.14	64.82	68.18	86.13
4	Hydrogen	wt. %	12.48	13.02	13.49	13.61	13.87
5	Oxygen	wt. %	49.93	34.73	21.59	18.15	0
6	Density at 15°C	kg/m ³	791.3	789.4	809.7	814.8	835
7	Viscosity at 40 °C	mm ² /s	0.58	1.13	2.22	2.89	2.72
8	Flash point	°C	11-12	17	35-37	49	>55
9	Boiling point	°C	647	78.3	117.5	137.9	180-360
10	Self-ignition temperature	°C	463	420	345	300	254-300
11	Lower calorific value (LCV)	MJ/kg	19.58	26.83	33.09	34.65	42.49
12	Cetane number	-	5	8	17	18.2-20	52
13	Solubility	g/L	Miscible	Miscible	77	22	Immiscible
14	LHV	kJ/kg	1162.64	918.42	585.40	308.05	270-375

along with rising the proportion of the alcohol inside the binary blend while HC figures increased drastically up to 40% in comparison with pure diesel. Based on the outcomes, the minimum BSFC and the peak BTE were detected with diesel fuel because of the LCV of diesel that is higher than that of isoamyl alcohol. The highest cylinder gas pressure and heat release rate of alcohol-treated fuel samples were attained to be higher than that of diesel fuel in the meantime the ignition delay duration prolonged with using diesel/alcohol blend contrary to the diesel fuel owing to the fusel oil's cetane number. Campos-Fernández et al. [52] conducted tests for a CI engine performance operating with the mixtures of long-chain alcohol/diesel, including between 10% and 25% 1-pentanol by volume. There was no significant variation in the power, BTE, and BSFC when the tested engine powered by the generality of the above-mentioned fuels in place of conventional diesel fuel. Furthermore, the conducted analysis validated insignificant alterations among the mixtures and diesel trials statistically. Accordingly, the researchers reported that 1-pentanol/diesel fuel blends could be taken into consideration to be suitable alternating fuel candidates providing that the emissions and long-term tests can give convenient findings. Santhosh et al. [53] tested 1-pentanol/diesel blends in the CI engine, having a common-rail injection, with the exhaust gas recirculation system so as to appear the emission and performance grades. Experimental findings showed that 30% 1-pentanol/70% diesel fuel led to a decline in BTE by 3.8%, a boosting in BSFC by 9.14%, a reduction in NO_x emission by 16.7%, and an insignificant rise in CO and HC emissions at 60% load. The authors mentioned that up to 30% higher-alcohol could be evaluated as alternatives to reference fuel though at the expense of performance. Ashok et al. [54] analyzed the impact of n-pentanol with *Calophyllum* oil methyl ester on characterizations in the unmodified CI engine. They used higher proportions of n-pentanol (up to 50%

by volume) in the biodiesel. On the other hand, the infusion of up to 30% n-pentanol to the biodiesel improved BTE by comparison diesel. A higher BTE was obtained with 10% n-pentanol/90% biodiesel blend by 27% that was lower than that of diesel. It was to be noticed that n-pentanol and biodiesel blends generated 33-50% and 15-43% decrement in the HC and CO emissions, respectively. Moreover, the smoke and NO_x emissions were observed to be lower for the alcohol added fuel samples when compared diesel. The researchers claimed that 10% n-pentanol supplementation to biodiesel had preferable characteristics on account of emission as well as engine performance. Sridhar and coworkers [55] investigated the influence of the infusion of 1-pentanol on the emission and performance behaviors of a single-cylinder CI engine fuelled with diesel and biodiesel fuels for six different loads (from 0 to 20 kg intervals of 4 kg). In the light of the experimental results, they indicated that 1-pentanol/diesel or biodiesel blends decreased the CO, HC, and NO_x concurrently contrary to straight diesel fuel meanwhile a little decline in BTE occurred in the binary blends. Since this investigation was performed only 20% of 1-pentanol addition to diesel fuel or biodiesel, further experiments were required to obtain the accurate effects of other mixtures on the performance and emissions profiles. Appavu et al. [56] recommended the diesel fuel/jatropha oil biodiesel/pentanol blend concerning a novel fuel mixture for the CI engine and researched the performance and emissions at various engine speeds between 1200-2800 rpm. They concluded that the 20% by volume pentanol addition to diesel fuel/jatropha oil biodiesel caused in lesser smoke, CO and NO_x emissions approximately by 32.4%, 41.76%, and 27.6%, respectively owing to the excessive quantity of oxygen molecules in the ternary mixtures leading to advance the combustion efficiency in the engine. Since pentanol possesses many advantages against short-chain alcohols, Yılmaz and Atmanlı [57] prepared various 1-

pentanol/diesel fuel blends which included 5%, 10%, 20%, 25%, and 35% alcohol. The researchers investigated the performance and emission features at several loads (0, 1.5, 2.25 and 3 kW) with a fixed speed (2000 rpm). To conclude with, 1-pentanol treated fuel specimens have resulted in higher CO and HC emissions as compared to diesel by virtue of the higher LHV of 1-pentanol leading a lesser exhaust gas temperature because of the quenching effect. However, the supplementation of 1-pentanol into diesel caused an increase in BSFC meanwhile EGT was positively affected.

It can be noticed from the extensive literature survey that there are restricted studies with respect to the utilization of 1-pentanol in the CI engine applications even though 1-pentanol is a type of long-chain alcohol, having better physicochemical characteristics as compared to lower alcohols because of the advantages of pentanol as highlighted above. Therefore, it can be clearly noted that this topic is necessary to be further researched so as to accomplish from these shortcomings placed in the literature. The aim of the present experimental work is to investigate the engine performance and exhaust emission characteristics of a single-cylinder diesel engine felled with straight diesel fuel and 1-pentanol/diesel fuel blends in which 1-pentanol is recently accepted as a next-generation alternative and clean fuel substitution. For the aforementioned perspective, 10%, 20%, and 30% by volume of 1-pentanol were blended with traditional diesel in order to achieve Pt10, Pt20, and Pt30 labeled fuel blends, respectively. The engine tests were carried out at fixed engine speed (3000 rpm) with variable loads (from no load to 2 kW at 0.4 kW intervals). The experimental outcomes were compared to the reference diesel and discussed with the results of the recent literature works.

2. Material and Method

2.1. Experimental setup

In experimental studies, there are instrument required for control and operation with 230/400 V brushless synchronous alternator in a generator set with a single-cylinder, naturally aspirated, and direct-injection (DI) diesel engine, the technical features of which were given in Table 2. The loading of the engine has been provided by the resistance module that consumes the electrical energy produced by the generator. In the module, General brand resistors, which have 200 and 1000 W capacities each of them, were used and the output power was calculated by using the values on the digital display of the integrated ammeter and voltmeters on the setup. In order to get the accurate and stable results, the engine was firstly brought to steady-state conditions by running for a particular time. Experimental studies were carried out for different engine loads by using pure diesel and 1-pentanol/diesel fuel mixtures in the test setup given in

Fig. 1. The impacts of these fuel samples on performance and exhaust emissions were examined.

Experimental studies were first done with Pt0 (neat diesel); performance parameters and exhaust emission levels were determined, and then tests were continued with Pt10, Pt20, and Pt30 fuels. Before starting the trials, the tested engine and emission measuring device had been checked. The tested engine was initially run for 15 minutes to reach a steady state status. Experimental studies have been performed on the engine brought to operating temperature at a fixed speed (3000 rpm) for six different load values (from 0 to 2 kW at intervals of 0.4 kW) using the test setup given in Fig. 1. Ambient temperature and humidity were constantly checked during the experiments. The temperature value was read from the indicator on the control panel. The temperatures were measured using the J type TMX-B12F08 model thermocouple, which can measure between -200 °C and 800 °C, attached to the exhaust manifold.

Table 2. Technical specifications of the engine and the generator used in the experiment

Diesel engine	
Parameters	Specifications
Brand	Katana
Model	Km 178 F
Number of cycle	4
Number of cylinder	1
Continuous power	6 hp
Maximum engine power	6.7 hp
Type of fuel	Diesel fuel
Type of ignition	Compression-ignition
Type of fuel injection	Direct-injection
Engine speed	3000 rpm
Swept volume	296 cm ³
Stroke	62 mm
Bore	78 mm
Cooling system	Air-cooled
Injector nozzle number	4
Fuel injection pressure	200 bar
Injection timing	20° before TDC
Intake system	Naturally-aspirated
Compression ratio	18:1
Generator	
Parameters	Specifications
Brand	Kama
Model	KDL3500CE
Maximum power	3 kW
Continuous power	2.7 kW
Phase	1
Voltage	230
Frequency	50 Hz
Current	11.6 A

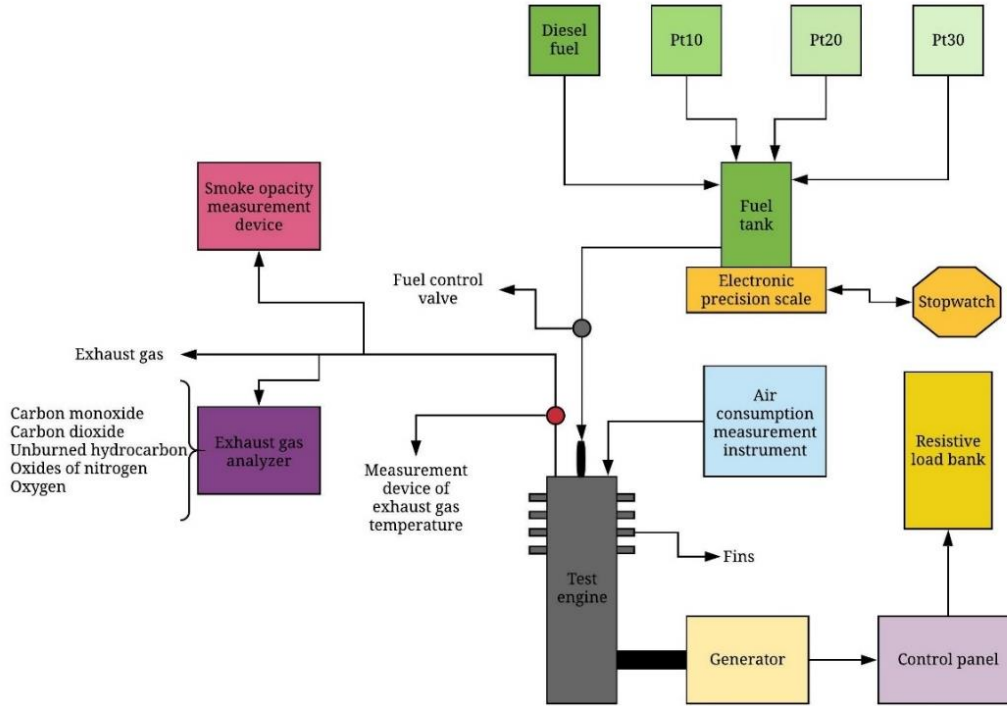


Fig. 1. Schematic layout of the experimental apparatus

The fuel consumption was measured in mass by using the Weithglab brand WH-2002 model electronic precision scale which can measure with an accuracy of 0.01 g and a digital stopwatch. The fuel tank was emptied and refilled with new tested fuel before each experimental study commence. In addition, the engine was let cool for a certain period of time prior to each new experimental study to prevent measurement errors for performance and exhaust emissions.

Exhaust gas emissions were measured according to the TS 11365-T1 standard by using the Bilsa brand MOD 2210 WINXP-K model exhaust gas analyzer. Information about the measurement range and sensitivity of this device is tabulated in Table 3.

Table 3. Technical specifications of the exhaust gas analyzer

Item	Measuring Range	Accuracy
CO (%)	0-10	0.001
CO ₂ (%)	0-20	0.001
HC (ppm)	0-10000	1
NO _x (ppm)	0-5000	1
O ₂ (%)	0-25	0.01
Lambda (λ)	0-5	0.001
Smoke (%)	0-100	0.1
Air/fuel ratio	5-30	-

The values of BTE, BSFC, and BSEC for all tested fuels were calculated from Eqs. (1-3) by using the data obtained

from the engine tests conducted in experimental studies [58, 59].

$$BTE = \frac{BP}{\dot{m}_f \times LCV_f} \times 100 \quad (1)$$

$$BSFC = \frac{3600 \times \dot{m}_f}{BP} \quad (2)$$

$$BSEC = \frac{BSFC \times LCV_f}{1000} \quad (3)$$

where,

BP (kW): brake power,

$\dot{m}_f$ (g/s): mass flow rate of the fuel,

LCV_f (MJ/kg): lower calorific value of the fuel.

2.2. Test fuels

Experimental studies were carried out by using 1-pentanol with diesel fuel. The fuel blends were prepared as 10% 1-pentanol + 90% diesel fuel (Pt10), 20% 1-pentanol + 80% diesel fuel (Pt20), and 30% 1-pentanol + 70% diesel fuel (Pt30) by volume. As a result of the examinations and observations, it was determined that phase separation has not been appeared in fuel blends until the end of the experimentations.

Some of the basic fuel properties (density, LCV, and ce-

tane number) of all tested blends composed of 1-pentanol and diesel have been predicted on account of the Kay's mixing rule technique represented by Lin et al [60] and Atmanli et al. [61]. Furthermore, the kinematic viscosity values of the 1-pentanol/diesel blends were estimated implementing Eq. (5) which was the Arrhenius type mixing rule [61, 62].

The Kay's mixing rule and Arrhenius type mixing rule may be mathematically referred as an underneath given forms:

$$y = \sum_i^n x_i \varphi_i \quad (4)$$

$$\ln \eta_b = \sum_i^n x_i \ln \eta_i \quad (5)$$

where,

x: concentration of the component,

y: esteemed property,

φ : corresponding property,

η : kinematic viscosity.

The main fuel properties for the diesel, Pt10, Pt20, Pt30, and 1-pentanol were tabulated in Table 4.

Table 4. The main fuel properties for the tested fuel samples used in this experimental work

No	Property	Unit	Diesel fuel	Pt10	Pt20	Pt30	1-pentanol
1	Chemical formula	-	C ₁₄ H ₂₅	C _{13.1} H _{23.7} O _{0.1}	C _{12.2} H _{22.4} O _{0.2}	C _{11.3} H _{21.1} O _{0.3}	C ₅ H ₁₂ O
2	Density ¹	g/cm ³	0.820	0.819	0.818	0.817	0.810
3	Kinematic viscosity ²	mm ² /s	2.416	2.457	2.500	2.542	2.863
4	Cetane number	-	53	50	46	43	20
5	LHV ³	kJ/kg	270-375	-	-	-	308.5
6	Molecular weight	g/mol	193.0	182.52	172.03	161.55	88.15
7	LCV	kJ/kg	43.168	42.474	41.981	40.987	34.632
8	Carbon	wt. %	87.05	86.14	85.12	83.96	68.18
9	Hydrogen	wt. %	12.95	12.98	13.02	13.07	13.64
10	Oxygen	wt. %	0	0.88	1.86	2.97	18.18
11	Carbon/Hydrogen	-	6.722	6.636	6.538	6.424	4.999
12	Copper strip corrosion ⁴	Degree of corrosion	1a	1a	1a	1a	-
13	Assay	%	-	-	-	-	99
14	Flash point	°C	60	58	55	40	48
15	Water content	ppm	12	90	179	271	858

¹at 15°C

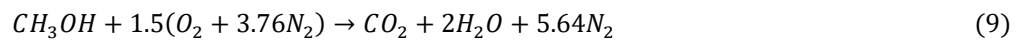
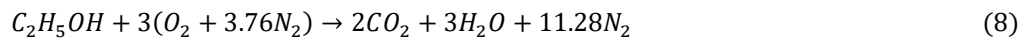
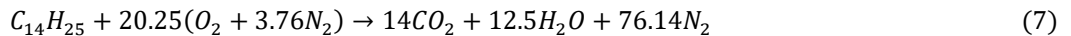
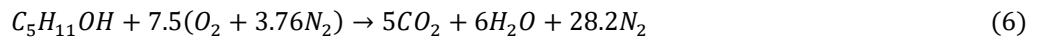
²at 40°C

³These values were adapted from Ref. [39].

⁴3 h at 50°C

The exact combustion equation of pentanol is given in Eq. (6). Accordingly, the air/fuel ratio for theoretical complete combustion is found to be at 11.7. Since the air/fuel ratio of pure diesel fuel calculated from Eq. (7) is 14.4, the amount of energy to be released under the same conditions will be more for diesel fuel. In other words, it needs to consumes more mixture fuel in mass in order to generate the identical effective power from the engine when compared to pure diesel [63-65]. Oxygen constitutes 34.8% and 50% of the

total molecular weight of ethanol and methanol, respectively. The air/fuel ratio for the theoretically complete combustion calculated from Eqs. (8) and (9) of ethanol and methanol is 8.95 and 6.44, respectively. The amount of oxygen that has no calorific value is high when it burns in the composition of both alcohols. For this reason, air should be well adjusted when using an alcohol-diesel fuel blends in diesel engines.



2.3. Uncertainty analysis

The accuracy of the measurement apparatus used in the experimental works can be calculated from the analysis of uncertainties of the equipments. In fact, the uncertainties have been principally revealed because of the calibration of the devices, observation by the researcher, environmental conditions, apparatus and system of the experiment progress techniques [66]. From this perspective, the uncertainty values of made use of the instruments in the present study such as exhaust gas emission sensors, temperature sensor, smoke meter, etc. were taken into consideration. Accordingly, it is to be mentioned that the uncertainties of the outcomes coming from the experimentations were predicted with respect to the square root method which were represented underneath [67, 68]. The percentage uncertainty values of the measured as well as the calculated parameters have been exhibited in Table 5.

$$w_R = \left[\left(\frac{\partial R}{\partial x_1} w_1 \right)^2 + \left(\frac{\partial R}{\partial x_2} w_2 \right)^2 + \dots + \left(\frac{\partial R}{\partial x_n} w_n \right)^2 \right]^{1/2} \quad (10)$$

where,

R: function of the independent variables,

$x_1, x_2, \dots, x_n$: Independent variables,

$w_1, w_2, \dots, w_n$: Uncertainties of independent variables,

w_R : Uncertainty of the results.

Table 5. The percentage uncertainty values of the measured as well as the calculated parameters

No	Item	Percentage uncertainty
1	Load	± 0.50
2	Engine speed	± 0.33
3	Fuel flow rate	± 1.11
4	Brake specific fuel consumption	± 1.27
5	Brake thermal efficiency	± 1.26
6	Exhaust gas temperature	± 0.50
7	CO	± 1.17
8	CO ₂	± 0.60
9	HC	± 0.82
10	NO _x	± 0.73
11	O ₂	± 0.60
12	Smoke opacity	± 0.62

3. Results and Discussion

In this section, the findings of the performance and exhaust emission characteristics for 1-pentanol/diesel binary blends have been presented and compared to a reference with mineral diesel fuel. Further, the aforementioned re-

sults have been discussed in the light of the recent literature.

3.1. Brake specific fuel consumption

BSFC can be described as the fuel consumption in a mass of the tested engine per unit output power generation. It is to be noted that BSFC is depended on the fuel properties such as density, viscosity, LCV, cetane number [69]. As a result of the tests in the study, the effects of the fuels obtained by adding 1-pentanol in different volumes to standard diesel fuel on BSFC were evaluated. The comparisons of the BSFC outcomes as a function of the load for the tested fuels during the experimental studies were portrayed in Fig. 2. As seen in Fig. 2, BSFC figures for all binary blends have been observed as elevated than that of diesel throughout the entire engine loads. BSFC values for 1-pentanol/diesel fuel blends have been noticed as higher than that of diesel fuel entire the engine loads. At the highest load, BSFC results for diesel, Pt10, Pt20, and Pt30 were calculated to be as 371.14 g/kWh, 390.95 g/kWh, 407.68 g/kWh, and 422.83 g/kWh, respectively. The increase in the concentration of 1-pentanol in the binary blend has led to a turn in up BSFC values. This is the fact that the 1-pentanol has a higher LHV value than that of diesel fuel (as observed in Table 4). Namely, the alcohol retracts more heat from the combustion chamber throughout the vaporization stage and hence, it brings about a quenching impact resulting in a decrement of the combustion efficiency. Due to the LCV of 1-pentanol compared to pure diesel (as observed in Table 4), the fuel consumption rises as the ratio of 1-pentanol ascends in the blends. As hoped, since the tested engine maintains the same amount of power generation, it consumes more fuel while operating with 1-pentanol/diesel fuel blends owing to the fact that 1-pentanol possesses a lesser heat of combustion. The similar results and their reasons were also found by Refs. [63, 70, 71].

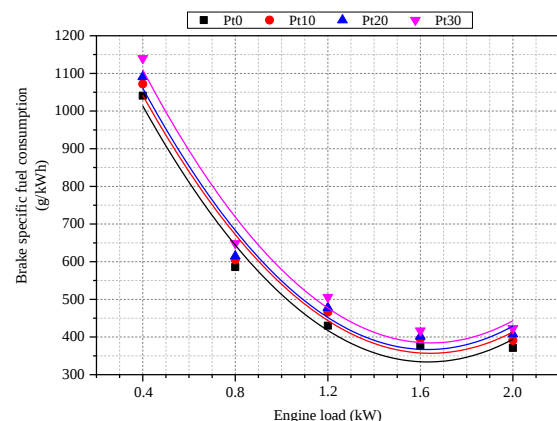


Fig. 2. The variations of BSFC according to different engine loads

3.2. Brake specific energy consumption

BSEC is an important indicator that is used to figure out the amount of energy consumption by the tested engine to the production of unit power. For this reason, it is clearly stated that the BSEC is a more reasonable parameter as compared to BSFC as mentioned above so as to compare any fuels having dissimilar heating values and densities. BSEC can be computed by multiplying the LCV of the tested fuel sample with BSFC result [72]. Fig. 3 illustrates the change in BSEC values on the influences of 1-pentanol infusion into the straight diesel fuel against the engine loads. The increase in the load caused to a mitigation in BSEC values. The possible reason for this case could be clarified that the number of required fuel running on the tested engine per unit output energy under the higher loads reduced [73]. As expected, it can be noticed that pure diesel fuel has the least BSEC values entire loads amongst the fuels by virtue of the LCVs and higher density of the 1-pentanol. The average BSEC values for diesel, Pt10, Pt20, and Pt30 were determined to be as 24.21 MJ/kWh, 24.88 MJ/kWh, 25.13 MJ/kWh, and 25.69 MJ/kWh, respectively. Particularly, the infusion of 1-pentanol with diesel fuel caused to increase the BSEC values at all engine loads. As mentioned before, the higher oxygen concentration in the alcohol has led to reduce the calorific value and therefore, the consumption of fuel boosts to generate the identical output of power from the tested engine. Ashok et al. [74] reported that the less calorific value, high boiling point, and viscosity characterization might be a conceivable ground in terms of increasing the BSEC. Babu and Anand [75] observed that the supplementation of n-hexanol or n-pentanol into the diesel/biodiesel fuel blends at ratios of 5% and 10% caused to increase BSEC values contrary to the diesel on account of the LCV of the alcohols than those of biodiesel and diesel fuel.

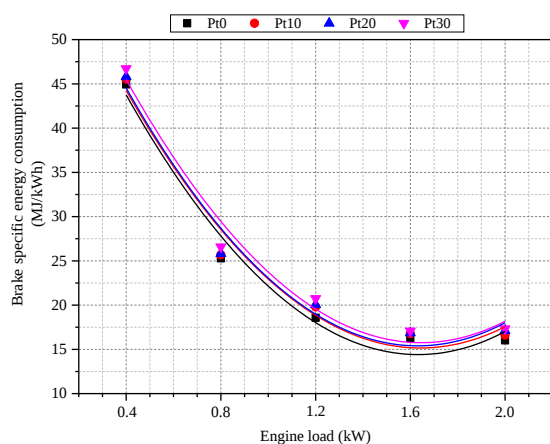


Fig. 3. The variations of BSEC according to different engine loads

3.3. Brake thermal efficiency

BTE has been known as an engine efficiency obtained by the rate of output power to input energy amount ensured from the fuel. It seems to be a very important parameter for the engine and generally used to predict how well any engine may transform the heat from any fuel to mechanical energy [72]. By all means, the BTE is the inverse of BSFC and LCV of the tested fuel [69]. BTE of the tested fuels operated in the engine trials was calculated thanks to Eq. (1) and given in Fig. 4 as a function of load. From the graph, BTE figures augmented with regards to the load for all fuel samples. To conclude with, the peak BTE figures were revealed at the highest load condition for all the fuels. At 2 kW, the BTE values of diesel, Pt10, Pt20, and Pt30 were found to be at 22.47%, 21.68%, 21.03%, and 20.77%, respectively. As the 1-pentanol ratio increases in the fuel blends, the BTE results decreases slightly. The basic reason for this is because LCV of 1-pentanol is lesser than that of pure diesel. Campos-Fernández et al. [52] and Wei et al. [63] stated that there was no change in BTE values against pentanol infusion to the diesel fuel. However, Yilmaz and Atmanli [57] highlighted that the treatment of diesel with pentanol exhibited sharp reductions in BTE values and 5-35% pentanol addition to diesel fuel exhibited average decrements of 13.85-22.98% in BTE results in contrast to the baseline diesel. Zhang et al. [76] indicated that a higher LHV of pentanol could decrease the combustion process temperature leading to a decline of the BTE. Kumar and Saravanan [77] observed that the BTE dropped in the engine while the utilization of pentanol/diesel fuel blends.

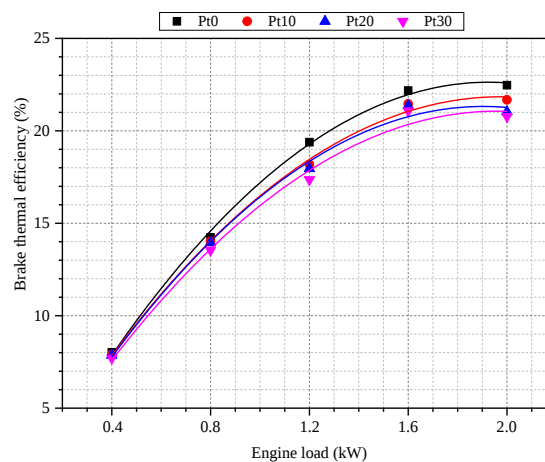


Fig. 4. The variations of BTE according to different engine loads

3.4. Exhaust gas temperature

With the help of an exhaust system in the diesel generator used in experimental studies, the products obtained at the end of the combustion were released into the atmosphere. One of the most remarkable characteristics of an engine that affect exhaust emissions is EGT. EGT results of the fuel samples under diverse loads are exhibited in Fig. 5. The highest EGT figures were obtained for all of the fuels with the raise of engine load. It was noticed that the injected number of fuel into the engine cylinder augments leading to a rise of temperature in the cylinder as the load increases [48, 78]. The amount of nitrogen oxides (NO_x) formed during the combustion process largely depends on the temperature. As a result of dilution of the fresh mixture in the combustion chamber with exhaust gases, the end of combustion temperatures can reduce and hence the amount of NO_x formation decreases. This subject would be elaborately presented in the related section giving the information regarding the NO_x formation mechanisms. It can be noted that the operating conditions of the test engine like injection pressure, compression ratio, fuel injection timing, etc. and fuel specifications such as energy content, cetane number, density, viscosity, etc. are mostly indicated as the most significant parameters for varying the EGT [79].

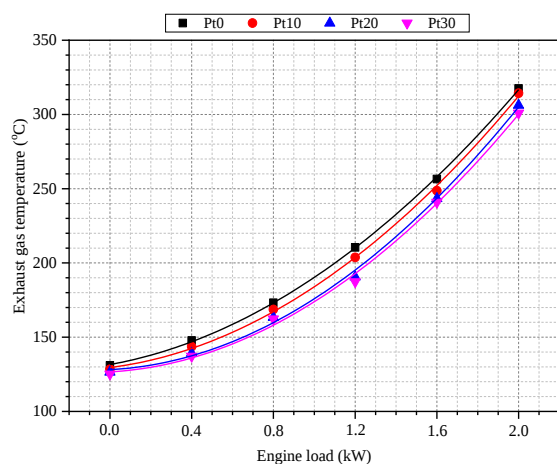


Fig. 5. The variations of EGT values according to different engine loads

With the infusion of alcohol to diesel fuel, EGT values commenced declining slightly in contrast to the diesel fuel. The peak EGT values for Pt10, Pt20, and Pt30 were measured to be as 314.3 °C, 306.2°C, and 300.9°C, respectively while the maximum EGT for diesel fuel was experienced as 317.5°C. Due to the higher LHV, there was a reduction in EGT values when the alcohol was added to the diesel fuel. As also mentioned above, the higher LHV can absorb the heat from the combustion chamber resulting in the drop of the end temperature [77]. Another important parameter for observing the reduction in EGT values for 1-pentanol/diesel blends in comparison with the straight diesel fuel is LCV.

As seen in Table 4, the 1-pentanol has lower energy content than that of diesel. Also, diesel fuel has the highest LCV amongst the tested fuel. It caused the production of more heat inside the cylinder and thereby EGT values observed as the maximum for diesel. Similarly, Wei et al. [63] marked that n-pentanol addition into diesel caused slight reductions in EGT values owing to the lower energy content and a higher LHV of the n-pentanol. Furthermore, similar scenarios were explained with the mixtures of diesel fuel with alcohol having various carbon atoms in the literature [80, 81]. Yilmaz and Atmanli [57] exhibited an opposing knowledge that the treatment of pure diesel fuel with higher alcohol (pentanol) led to a reduction in the cetane number owing to the less cetane number of alcohol, resulting in the rise of EGTs. Furthermore, the excessive amount of oxygen molecule found in the alcohol could positively influence the combustion efficiency in the engine and thus in the meantime associate with the raise in the EGT.

3.5. Carbon dioxide emission

In recent years, international protocols have been prepared to mitigate the harmful exhaust emissions to the environment from vehicles powered with internal combustion engines. Consequently, harmful pollutants are expected to be lower in the usage of alternative fuels that will become a candidate for petroleum products. CO_2 emission changes for the tested fuels obtained in the present experimental studies are demonstrated in Fig. 6. From the graph, CO_2 emission is the highest value for all 1-pentanol/diesel fuel blends and neat diesel at the load of 1.2 kW. The peak CO_2 emissions for diesel, Pt10, Pt20, and Pt30 were detected to be at 2.31%, 2.24%, 1.72%, and 1.50%, respectively. When Eqs. (6) and (7) are examined, it has been seen that the carbon atoms in the chamber of the combustion are oxidized with a sufficient amount of oxygen to form the complete combustion product that is CO_2 emission, which is known as the responsible for the greenhouse gas resulting in global warming [82]. All the tested fuels exhibited almost similar inclination in the CO_2 profile across the load. CO_2 generated by biomass-based alternative fuels does not have a negative impact on the environment since the released CO_2 gas can be used by plants in the course of the photosynthesis process during growth [83]. This means briefly net-zero carbon emission from the engine if it can operate with the above mentioned clean fuels like pentanol [84]. As reported before, the pentanol can be produced from biomass resources. As seen, the tested engine formed more CO_2 emissions for all the engine loads when it was fuelled with diesel fuel. But, CO_2 emissions were gradually reduced by adding 1-pentanol into the diesel fuel and thereby the lowest results were appeared with Pt30 blend fuel. It could be noted as the 1-pentanol amount in the blends rose progressively, the generation of CO_2 in the exhaust reduced. This case can be explained as the cooling influence of the 1-pentanol leading

inefficient oxidation process of carbon monoxide to dioxide inside the cylinder. Also, CO_2 formation in the end-combustion products also depends on the C/H ratio of fuels. Raising the mass of carbon atoms in the fuel content causes CO_2 ratio in the exhaust gas to increase. Nanthagopal et al. [72] observed that the higher-order alcohol addition to the methyl ester obtained from oil of *Calophyllum* brought about the declining CO_2 emissions according to the pure methyl ester fuel throughout the operation of the tested engine. This is because of higher amounts of oxygen atoms and hydrogen molecules in the chemical structures of the alcohol and hence the generation of CO_2 reduced. Akar [85] tested diesel fuel/butanol/false flax biodiesel ternary blends in the CI engine. The researcher accomplished that the higher-order alcohol supplementation into diesel/biodiesel blend resulted in decreasing for the perspective of the CO_2 emissions. A similar decrement was also indicated by Alptekin et al. [86] who pointed out that CO_2 emission for the 20% bioethanol/60% diesel/20% waste cooking oil biodiesel ternary blends gone down up to 7.1% when compared to diesel under 600 Nm load because of lesser C/H proportion of the bioethanol.

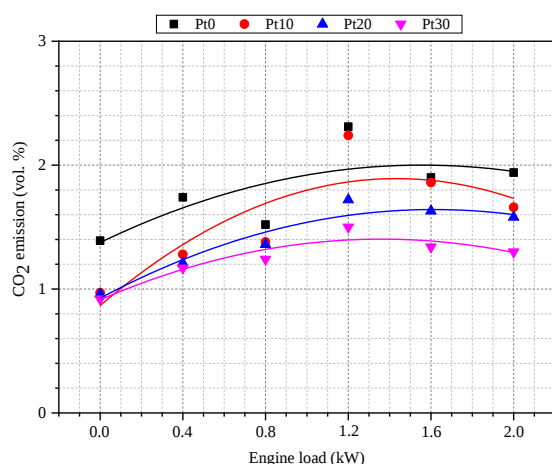


Fig. 6. The variations of CO_2 emissions for all tested fuels in different engine loads

3.6. Carbon monoxide emission

In cases where the carbon atoms cannot react with a sufficient amount of oxygen during the combustion, CO is formed that the indicator of the incomplete combustion process in the cylinder. The shortage of oxygen molecule concentration inside the cylinder and excessively lean or rich mixtures causes a higher CO generation [61]. The influence of pure diesel and 1-pentanol/diesel blends on CO emissions is presented in Fig. 7. As observed, the larger proportion of alcohol in the fuel blends results in higher CO emissions throughout all of the engine loads, especially at the higher loads. At 2 kW engine load, the CO emissions for diesel fuel, Pt10, Pt20, and Pt30 were found to be at

0.10%, 0.19%, 0.45%, and 0.70%, respectively. Although the number of carbon atom in the chemical structure of 1-pentanol is less than that of pure diesel, CO emissions are higher in 1-pentanol/diesel fuel blends. The highest value for the CO emission was obtained by the Pt30 fuel at all engine load conditions. Accordingly, these findings were compatible with the results of experiments performed by Refs. [63, 87, 88]. Kumar and Saravanan [77] indicated that the higher LHV feature of pentanol led to withdrawn a higher amount of heat from the chamber of combustion, as a result of the quenching impact, leading descend in the combustion efficiency of the tested engine and hence the generation of CO emission increased. No doubt, the temperature of the intake air sucked to the cylinder could be increased to overcome and mitigate the CO emissions [89]. Yilmaz and Atmanli [57] indicated that the low cetane number for pentanol could be a substantial parameter in the rising of CO emissions. On the other hand, the researchers presented that the low fraction (5% by volume) of pentanol addition to diesel fuel occurred an opposing trend on the emissions of CO. In other words, 5% pentanol + 95% diesel fuel blend ensured a decrement in CO emission by 16.39% on average when compared to diesel. But, CO emissions were augmented related to the increase in the concentration (between 10% and 35%) of pentanol in the blend. Nanthagopal et al. [72] pointed out that the higher-order alcohol (1-butanol and 1-pentanol)/biodiesel blends produced more CO emissions from the exhaust for all loads on account of the higher LHV as well as worse ignition features of the aforementioned long-chain alcohols resulting in the incomplete combustion reaction inside the cylinder and hence higher amount of CO emissions could be formed. Kumar et al. [90] noticed that the formation of CO gas in the blends of long-chain alcohol with diesel fuel or biodiesel has been heavily dependent on the content of the carbon atoms in the fuel samples. Namely, the rise in the number of carbon atoms would raise CO emissions owing to the declining in the oxygen fraction.

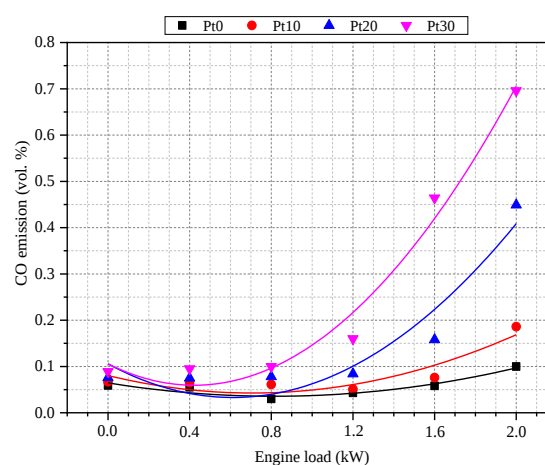


Fig. 7. The variations of CO emissions for all tested fuels in different engine loads

3.7. Unburned hydrocarbon emission

One of the most significant parameters for observing the quality of the combustion taking place inside the engine cylinder is unburned HC emissions. HC emissions occur because of not only the uncompleted combustion reaction but also slower oxidation process due to the very rich or poor air/fuel ratios in the combustion chamber, loss of heat to low-temperature zones around the cylinder, and cooling flame in the above-mentioned zones [91, 92]. Fig. 8 portrays the comparison of unburned HC emissions for the tested fuel samples (diesel and 1-pentanol/diesel blends) across the various engine load conditions. Unburned HC emissions obtained by using 1-pentanol/diesel fuel blends are higher than that of neat diesel as seen in Fig. 8. Besides, the maximum unburned HC emissions for all tested fuels were appeared under the highest load of 2 kW, and further at this load, the unburned HC emissions for Pt10, Pt20, and Pt30 were obtained to be as 259 ppm, 352 ppm, and 399 ppm, respectively. The unburned HC emission for unmodified diesel fuel was measured to be as 180 ppm. This substantial boosting is a good agreement with the raise in CO emissions, as observed in Fig. 7.

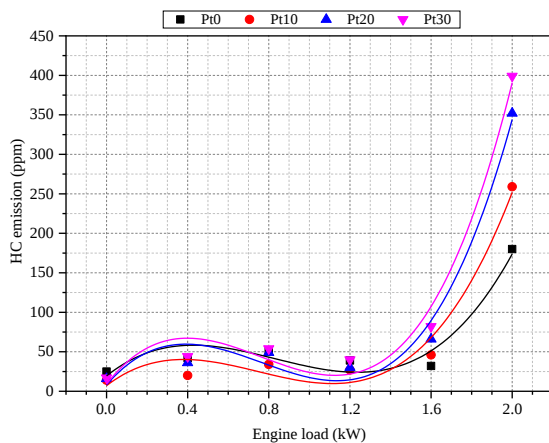


Fig. 8. The variations of HC emissions for all tested fuels in different engine loads

Increasing the amount of oxygen in 1-pentanol/diesel fuel mixtures affects increasing the combustion rate and temperature. Since the cetane number of 1-pentanol is lesser than that of pure diesel, it causes a prolong of ignition delay duration in the combustion reaction. Incomplete combustion formed due to the sudden combustion reaction of the fuel accumulated in the cylinder and shortening of the combustion period increases HC emissions [77]. Moreover, the low cetane number characteristic of the fuel is influenced by the specifications of the spray and volatility of the fuel, and low-temperature combustion chemistry as well [93]. Sharon et al. [82] and Kumar et al. [90] pointed out that the higher LHV of the pentanol caused to drop the temperature of the cylinder because of the cooling effects, which result-

ed in contributing to the augmentation of the generation of unburned HC emissions. Karabektas and Hosoz [81] observed that the addition of 5-20% isobutanol to diesel caused an increase in HC emissions by between 12.9 and 32.9% as compared to diesel. Yilmaz and Atmanli [57] found that 5%, 10%, 20%, 25%, and 35% by volume pentanol addition to the diesel fuel revealed increments to be as in the order of 16.63%, 45.55%, 97.78%, 182.10%, and 379.48% on average. Atmanli and Yilmaz [94] researched the influences of 1-pentanol and n-butanol infusion on the diesel for the emission levels. Based on the measurements, the researchers stated that the tested binary blends occurred a rise of 283.39% averagely in the unburned HC emissions. Contrary to the aforementioned outcomes, Altun et al. [95] observed reductions in the HC emissions with the rise in the higher-alcohol (butanol) concentration in the blend.

3.8. Nitrogen oxides emissions

The air consists of N_2 at a ratio of approximately 78% and this gas accepts as the inert gas. In other words, N_2 cannot react with the oxygen molecules in normal cases. On the other hand, N_2 can react with oxygen molecules associated with the elevated temperature in the combustion chamber. NO_x are formed by the nitrogen monoxide (NO) and nitrogen dioxide (NO_2). In the NO_x , a higher amount of NO gas (approximately 90% by volume) and a lesser amount of NO_2 gas (approximately 5% by volume) are found in general [57]. Moreover, the other oxides of nitrogen (NO_3 , N_2O_5 , N_2O , etc.) are not considered while determining the NO_x emissions. Nitrogen oxides (NO_x) emissions occur in the cylinder due to reasons such as high pressure, temperature, and excess oxygen quantity during the combustion process in the engine [96]. The understanding of the formation mechanisms for the NO_x emissions can be mentioned as a significant subject in the emission analysis in the point of the mitigating of the NO_x emission emitting from the CI engines. Zeldovich or thermal, Fenimore or prompt, the NNH, fuel-bound nitrogen, and N_2O pathway have been known as the most widespread NO_x formation mechanisms used in the literature [97]. However, the NO_x formation mechanism in the CI engines is commonly identified by the Zeldovich mechanism from the availability of nitrogen, oxygen, and hydrogen free radicals. The general equations of the aforementioned mechanism are represented underneath [98].



Fig. 9 shows the alteration of the NO_x emission figures for all the tested fuel samples under various loads. The av-

average NO_x emissions for diesel, Pt10, Pt20, and Pt30 were determined to be as 165.80 ppm, 143.53 ppm, 115.76 ppm, and 96.82 ppm, respectively. As observed, the NO_x emission values of the different blends in the diesel engine generator used in the study decreased depending on the increase in the amount of 1-pentanol. LCV and higher LHV of the 1-pentanol compared to that of pure diesel fuel led to decrease the occurrence of the NO_x emission. Since the air/fuel ratio in the cylinder will increase with the increase in load, the gas temperature increases in the combustion chamber. In other words, the utilization of pentanol in the diesel fuel as an oxygenated alternative fuel additive reduces the temperature of the engine cylinder throughout the combustion process by causing the leaner air/fuel mixture and hence decreases the NO_x emissions [20]. The lowest value for the NO_x emission was obtained by the Pt30 blend fuel all of the engine load conditions. EGT increase with the increase of load, NO_x emission values were increased in all fuel blends as seen in Figs. 5 and 9. The main reason for this is the decreased rate of heat transfer through the coolant in the cylinder wall. Mahalingam et al. [99] found that the adding 10% and 20% by volume pentanol to mahua oil biodiesel caused to 3.3% and 3.9% mitigation in the emissions of NO_x , respectively. The NO_x emission forms during the combustion of diesel fuel and is the most important contaminant component that must be controlled. Devarajan et al. [47] stated that the NO_x emissions could be pushed down by decreasing the combustion temperature. However, the researchers observed that the addition of pentanol to cashew nut shell biodiesel resulted in higher NO_x emissions than that of diesel entire brake power conditions because of the inherent oxygen content in the biofuels leading to encourage the combustion and therefore turn in up the temperature inside the cylinder. Shu et al. [100] suggested that the pilot injection postponing might be a powerful technique so as to drop the NO_x formation of a CI engine fuelled with the natural gas/diesel blend.

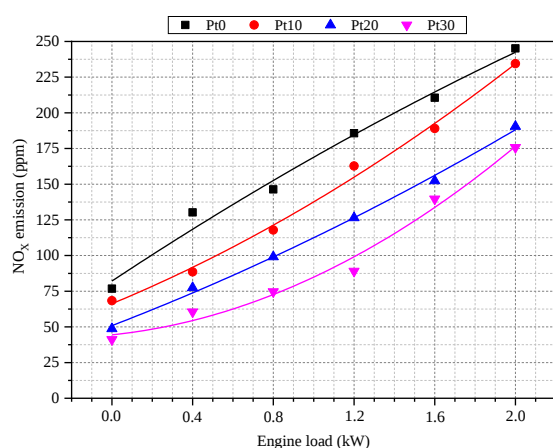


Fig. 9. The variations of NO_x emissions for all tested fuels in different engine loads

3.9. Oxygen emission

One of the most substantial factors ensuring the complete combustion in the combustion chamber is the proportion of the oxygen atoms in the cylinder. During the combustion process, the carbon atoms in the fuel chemical structure react with the oxygen atoms in the air. As a result of the utilization of alcohol-based fuels with oxygen atoms in its chemical structure, the oxygen emission during combustion increases in diesel engines. Oxygen emission emitted from the tested engine changes obtained in experimental studies is given in Fig. 10. The oxygen emission of 1-pentanol/diesel fuel blends is higher than that of pure diesel because of the inherent oxygen content of 1-pentanol. The average oxygen emission for the diesel fuel, Pt10, Pt20, and Pt30 were found to be at 18.21%, 18.57%, 19.04%, and 19.23%, respectively. To the best of the authors' knowledge, a limited number of researcher studied the oxygen emissions during the engine tests. Aydın and Ogut [38], for instance, investigated the oxygen emissions of the test engine fuelled with bioethanol/biodiesel/diesel fuel blends. The researchers noticed that the addition of bioethanol caused to increase the oxygen emissions in comparison with traditional diesel fuel because of the excessive amount of oxygen molecules in the bioethanol. Yesilyurt et al. [101] have observed that the infusion of long-chain alcohols like 1-butanol and n-pentanol to the yellow mustard oil biodiesel/diesel fuel blends at ratios of 5 and 10% on a volume basis resulted in turn up the oxygen emissions by averagely 84.62-121.34% for 1-butanol added fuel blends, and 52.74-78.38% for n-pentanol treated alternativefuel blends in comparison with the conventional diesel.

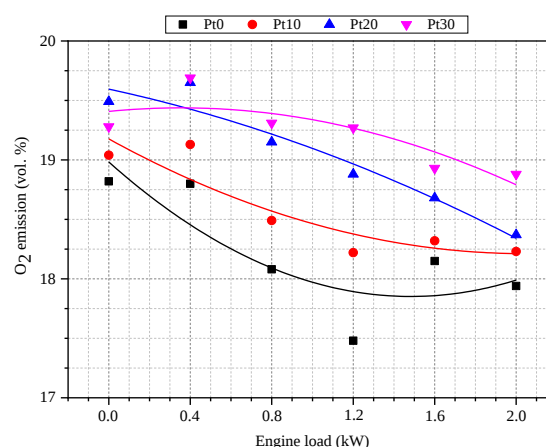


Fig. 10. The variations of oxygen emissions for all tested fuels in different engine loads

3.10. Smoke opacity

Fig. 11 portrays the alteration of smoke emissions for Pt10, Pt20, Pt30, and mineral diesel fuel against engine load between no load to 2 kW. As seen, the smoke emissions increase in most case with load for all tested fuel samples. This is due to the fact that a supplemental amount of fuel can be required with the identical number of air in the combustion chamber where makes the air/fuel ratios as a rich and leads to becoming incomplete combustion process and thereby higher smoke emissions in the exhaust [102]. The unmodified diesel fuel formed more smoke than that of the binary blends of 1-pentanol and diesel fuel. This can be mainly explained as the atomization stages of air has been enhanced by using the oxygenated fuel additives. At the highest load, smoke emissions for diesel, Pt10, Pt20, and Pt30 were noted to be at 59.78%, 13.16%, 8.54%, and 7.14%, respectively. Another reason for improvement of the smoke emissions by the utilization of 1-pentanol can be mentioned by the intensification of oxygen molecule fraction due to the alcohol [103]. Rakopoulos et al. [104] researched the influences of butanol/diesel blends on the exhaust gas emissions of a DI diesel engine under various loads and they reported that the smoke emissions were drastically decreased with the addition of butanol to diesel fuel. Emiroğlu and Şen [105] indicated that the use of alcohol in the diesel fuel decreased in the smoke emission levels due to the higher content of the oxygen and lesser C/H of the alcohol-based alternative fuels. With the above-mentioned perspective, the 1-pentanol has 4.999 C/H ratio while diesel fuel has 6.722 in the present study, as tabulated in Table 4. Therefore, the 1-pentanol addition to diesel fuel caused to drop the smoke emission grades in the exhaust gas. Moreover, these findings are also similar to other investigations conducted by Refs [28, 106, 107].

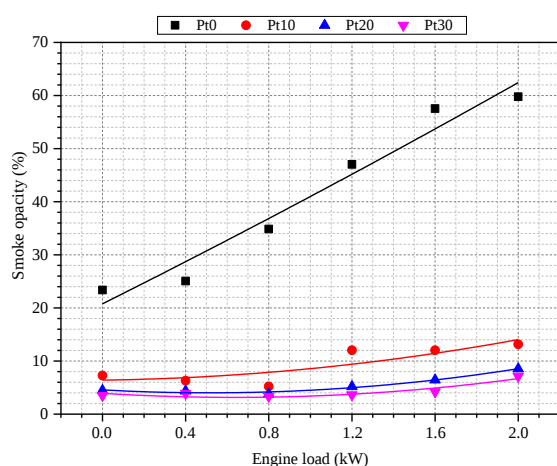


Fig. 11. The variations of smoke emissions for all tested fuels in different engine loads

4. Conclusions

In the present experimental study, the effects of different 1-pentanol/diesel fuel blends (Pt10, Pt20, and Pt30) on the engine performance and exhaust emission characteristics have been researched at a constant engine speed of 3000 rpm for six different engine loads (from no load to 2 kW intervals of 0.4 kW) in a single-cylinder, four-stroke, naturally-aspirated, DI diesel engine and the outcomes have been compared with the conventional diesel fuel. Based on the engine test of the aforementioned fuel samples, the following conclusions have been drawn from this work.

1. The most significant benefit of 1-pentanol/diesel fuel blends is to be noted that this higher-order alcohol could be successfully and safely performed in a CI engine coupled with a generator out of any modification on the tested engine along without any extra additive.
2. The 1-pentanol infusion with straight diesel fuel caused to decline of the energy content along with the cetane number of the tested fuel samples. Accordingly, Pt30 showed the lowest cetane number and calorific value amongst the tested fuels. The higher content of oxygen in the 1-pentanol leads to decrease the energy content. With this, in comparison to pure diesel fuel under the same experimental conditions, it has been observed that the BSFC and BSEC values increased as the amount of 1-pentanol increased in the blends. The order from least to utmost was as follows: diesel fuel < Pt10 < Pt20 < Pt30.
3. The being of 10%, 20%, and 30% by volume 1-pentanol in the fuel blends has turned down the EGT values when compared to the unmodified diesel fuel. The EGT values of Pt10, Pt20, and Pt30 blends were found to be lower than the of diesel by 2.35%, 5.44%, and 6.9% on average, respectively, which can be attributed to the higher LHV feature of the 1-pentanol than that of diesel fuel.
4. 1-pentanol/diesel fuel blends generated a higher amount of CO emission than diesel fuel owing to the higher LHV of used alcohol. In addition, the use of the above mentioned alternative fuel blends in the tested engine led to reducing the formation of CO₂ emission in the exhaust. It is clear that the formation of CO₂ gas from the burning of biomass-based fuel candidates has negligible because the emitting CO₂ can be absorbed by plants throughout the process of photosynthesis.
5. The utilization of 1-pentanol with diesel fuel at various ratios augmented the unburned HC emissions as compared to the diesel fuel, which gener-

- ated the lowest HC emission, because of the poor self-ignition characterizations of the tested fuel blends owing to lesser cetane number resulting in the cooling effect in the combustion chamber, especially leaner mixture regions inside the cylinder.
6. The usage of 1-pentanol with diesel fuel caused to release more oxygen emission from the exhaust because of the inherent oxygen content of the alcohol. The oxygen emission levels for the tested fuels were observed to be between 18.21% and 19.23%.
 7. The existence of 10%, 20%, and 30% on a volume basis 1-pentanol in the blends reduced NO_x emissions in comparison with diesel by 13.43%, 30.18%, and 41.61%, respectively.
 8. The addition of 1-pentanol to diesel fuel was appeared that it provided a noticeable reduction in the smoke opacity. The smoke emissions for diesel fuel, Pt10, Pt20, and Pt30 were measured to be as 59.78%, 13.16%, 8.54%, and 7.14%, respectively at the highest load.

Overall, it can be stated that the binary blends of 1-pentanol, which is an important higher-order alcohol, with diesel would be a possible and feasible substitute for baseline diesel fuel in the points of the short-term practices in a diesel engine. On the other hand, prior to intend for using the aforementioned blends as an alternative fuel candidate for the CI engine applications, plenty of systematical investigation has to be performed in the long-term durability and reliability aspects. By all means, there is a necessary for a lot of innovative procedures in order to obtain the long-chain alcohols from renewable and sustainable resources.

Nomenclature

$C_{14}H_{25}$	: Diesel fuel
$C_5H_{12}O$	: Pentanol
CI	: Compression-ignition
CO_2	: Carbon dioxide
CO	: Carbon monoxide
DI	: Direct-injection
SO_2	: Sulfur dioxide
HC	: Hydrocarbon
LPG	: Liquefied petroleum gas
CNG	: Compressed natural gas
NO_x	: Nitrogen oxides
NO	: Nitrogen monoxide

NO_2	: Nitrogen dioxide
O_2	: Oxygen
$OAPEC$	: Organization of Arab Petroleum Exporting Countries
$Pt0$	: 100% diesel fuel
$Pt10$	: 10% 1-pentanol + 90% diesel fuel
$Pt20$	: 20% 1-pentanol + 80% diesel fuel
$Pt30$	: 30% 1-pentanol + 70% diesel fuel
BTE	: Brake thermal efficiency
$BSFC$	: Brake specific fuel consumption
$BSEC$	: Brake specific energy consumption
$IMEP$	: Indicated mean effective pressure
IDI	: Indirect-injection
BP	: Brake power
EGT	: Exhaust gas temperature
LHV	: Latent heat of vaporization
$\dot{m}_f$	: Mass flow rate of the fuel
LCV_f	: Lower heating value of the fuel
x	: Concentration of the component
y	: Esteemed property
η	: Kinematic viscosity
ϕ	: Corresponding property
$x_1, x_2, \dots, x_n$	: Independent variables
$w_1, w_2, \dots, w_n$	: Uncertainties of independent variables
w_R	: Uncertainty of the results
R	: Function of the independent variables

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